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## APPENDIX A5—BASIC STEPS FOR CONCRETE BRIDGES

### A5.1—GENERAL

This outline is intended to be a generic overview of the design process using the simplified methods for illustration. It should not be regarded as complete, nor should it be used as a substitute for a working knowledge of the provisions of this section.

### A5.2—GENERAL CONSIDERATIONS

- A. Design Philosophy (1.3.1)
- B. Limit States (1.3.2)
- C. Design Objectives and Location Features (2.3) (2.5)

### A5.3—BEAM AND GIRDER SUPERSTRUCTURE DESIGN

- A. Develop General Section
  - 1. Roadway Width (Highway-Specified)
  - 2. Span Arrangements (2.3.2) (2.5.4) (2.5.5) (2.6)
  - 3. Select Bridge Type
- B. Develop Typical Section
  - 1. Precast P/S Beams
    - a. Top Flange (5.12.3.2.2)
    - b. Bottom Flange (5.12.3.2.2)
    - c. Webs (5.12.3.2.2)
    - d. Structure Depth (2.5.2.6.3)
    - e. Minimum Reinforcement (5.6.7) (5.6.3.3)
    - f. Lifting Devices (5.12.3.2.3)
    - g. Joints (5.12.3.4.2)
  - 2. CIP T-Beams and Multiweb Box Girders (5.12.3.5)
    - a. Top Flange (5.12.3.5.1a)
    - b. Bottom Flange (5.12.3.5.1b)
    - c. Webs (5.12.3.5.1c)
    - d. Structure Depth (2.5.2.6.3)
    - e. Reinforcement (5.12.3.5.2)
      - (1) Minimum Reinforcement (5.6.3.3) (5.6.7)
      - (2) Temperature and Shrinkage Reinforcement (5.10.6)
    - f. Effective Flange Widths (4.6.2.6)
    - g. Strut-and-Tie Areas, if Any (5.8.2)
- C. Design Conventionally Reinforced Concrete Deck
  - 1. Deck Slabs (4.6.2.1)
  - 2. Minimum Depth (9.7.1.1)
  - 3. Empirical Design (9.7.2)
  - 4. Traditional Design (9.7.3)
  - 5. Strip Method (4.6.2.1)
  - 6. Live Load Application (3.6.1.3.3) (4.6.2.1.5)
  - 7. Distribution Reinforcement (9.7.3.2)
  - 8. Overhang Design (A13.4) (3.6.1.3.4)
- D. Select Resistance Factors  
Strength Limit State (Conventional) (5.5.4.2)
- E. Select Load Modifiers
  - 1. Ductility (1.3.3)
  - 2. Redundancy (1.3.4)
  - 3. Operational Importance (1.3.5)
- F. Select Applicable Load Combinations and Load Factors (3.4.1, Table 3.4.1-1)
- G. Calculate Live Load Force Effects
  - 1. Live Loads (3.6.1) and Number of Lanes (3.6.1.1.1)
  - 2. Multiple Presence (3.6.1.1.2)
  - 3. Dynamic Load Allowance (3.6.2)
  - 4. Distribution Factor for Moment (4.6.2.2.2)



- a. Interior Beams with Concrete Decks (4.6.2.2.2b)
  - b. Exterior Beams (4.6.2.2.2d)
  - c. Skewed Bridges (4.6.2.2.2e)
- 5. Distribution Factor for Shear (4.6.2.2.3)
  - a. Interior Beams (4.6.2.2.3a)
  - b. Exterior Beams (4.6.2.2.3b)
  - c. Skewed Bridges (4.6.2.2.3c, Table 4.6.2.2.3c-1)
- 6. Reactions to Substructure (3.6)
- H. Calculate Force Effects from Other Loads as Required
- I. Investigate Service Limit State
  - 1. P/S Losses (5.9.3)
  - 2. Stress Limitations for P/S Tendons (5.9.2.2)
  - 3. Stress Limitations for P/S Concrete (5.9.2.3)
    - a. Before Losses (5.9.2.3.1)
    - b. After Losses (5.9.2.3.2)
  - 4. Durability (5.14)
  - 5. Crack Control (5.6.7)
  - 6. Fatigue, if Applicable (5.5.3)
  - 7. Deflection and Camber (2.5.2.6.2) (3.6.1.3.2) (5.6.3.5.2)
- J. Investigate Strength Limit State
  - 1. Flexure
    - a. Stress in P/S Steel—Bonded Tendons (5.6.3.1.1)
    - b. Stress in P/S Steel—Unbonded Tendons (5.6.3.1.2)
    - c. Flexural Resistance (5.6.3.2)
    - d. Limits for Reinforcement (5.6.3.3)
  - 2. Shear (Assuming No Torsional Moment)
    - a. General Requirements (5.7.2)
    - b. Sectional Design Model (5.7.3)
      - (1) Nominal Shear Resistance (5.7.3.3)
      - (2) Determination of  $\beta$  and  $\theta$  (5.7.3.4)
      - (3) Longitudinal Reinforcement (5.7.3.5)
      - (4) Transverse Reinforcement (5.7.2.3) (5.7.2.5) (5.7.2.4) (5.7.2.6)
      - (5) Horizontal Shear (5.7.4)
- K. Check Details
  - 1. Cover Requirements (5.10.1)
  - 2. Development Length—Reinforcement (5.10.8.1) (5.10.8.2)
  - 3. Development Length—Prestressing (5.9.4.3)
  - 4. Splices (5.10.8.4) (5.10.8.5)
  - 5. Anchorage Zones
    - a. Post-Tensioned (5.9.5.6)
    - b. Pretensioned (5.9.4.4)
  - 6. Ducts (5.4.6)
  - 7. Tendon Profile Limitation
    - a. Tendon Confinement (5.9.5.4)
    - b. Curved Tendons (5.9.5.4)
    - c. Spacing Limits (5.9.5.1)
  - 8. Reinforcement Spacing Limits (5.10.3)
  - 9. Transverse Reinforcement (5.7.2.4) (5.7.2.6) (5.7.2.7)
  - 10. Beam Ledges (5.8.4.3)

#### A5.4—SLAB BRIDGES

Generally, the design approach for slab bridges is similar to beam and girder bridges with some exceptions, as noted below.

- A. Check Minimum Recommended Depth (2.5.2.6.3)
- B. Determine Live Load Strip Width (4.6.2.3)
- C. Determine Applicability of Live Load for Decks and Deck Systems (3.6.1.3.3)
- D. Design Edge Beam (9.7.1.4)
- E. Investigate Shear (5.12.2.1)
- F. Investigate Distribution Reinforcement (5.12.2.1)

- G. If Not Solid
  - 1. Check if Voided Slab or Cellular Construction (5.12.2.2.1)
  - 2. Check Minimum and Maximum Dimensions (5.12.2.2.1)
  - 3. Design Diaphragms (5.12.2.2.3)
  - 4. Check Design Requirements (5.12.2.2.4)

**A5.5—SUBSTRUCTURE DESIGN**

- A. Establish Minimum Seat Width (4.7.4.4)
- B. Compile Force Effects Not Compiled for Superstructure
  - 1. Wind (3.8)
  - 2. Water (3.7)
  - 3. Effect of Scour (2.6.4.4.2)
  - 4. Ice (3.9)
  - 5. Earthquake (3.10) (4.7.4)
  - 6. Temperature (3.12.2) (3.12.3) (4.6.6)
  - 7. Superimposed Deformation (3.12)
  - 8. Ship Collision (3.14) (4.7.5)
  - 9. Vehicular Collision (3.6.5)
  - 10. Braking Force (3.6.4)
  - 11. Centrifugal Force (3.6.3)
  - 12. Earth Pressure (3.11)
- C. Analyze Structure and Compile Load Combinations
  - 1. Table 3.4.1-1
  - 2. Special Earthquake Load Combinations (3.10.8)
- D. Design Compression Members (5.6.4)
  - 1. Factored Axial Resistance (5.6.4.4)
  - 2. Biaxial Flexure (5.6.4.5)
  - 3. Slenderness Effects (4.5.3.2.2) (5.6.4.3)
  - 4. Transverse Reinforcement (5.6.4.6)
  - 5. Shear (Usually EQ and Ship Collision Induced) (3.10.9.4.3)
  - 6. Reinforcement Limits (5.6.4.2)
  - 7. Bearing (5.6.5)
  - 8. Durability (5.14)
  - 9. Detailing (as in Step A5.3K) and Seismic (5.11)
- E. Design Foundations (Structural Considerations)
  - 1. Scour
  - 2. Footings (5.12.8)
  - 3. Abutments (Section 11) (5.12.9)
  - 4. Pile Detailing (5.12.9)



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## APPENDIX B5—GENERAL PROCEDURE FOR SHEAR DESIGN WITH TABLES

### B5.1—BACKGROUND

The general procedure herein is an acceptable alternative to the procedure specified in Article 5.7.3.4.2. The procedure in this Appendix utilizes tabularized values of  $\beta$  and  $\theta$  instead of Eqs. 5.7.3.4.2-1, 5.7.3.4.2-2, and 5.7.3.4.2-3. Appendix B5 is a complete presentation of the general procedures in LRFD Design (AASHTO 2007) without any interim changes.

### B5.2—SECTIONAL DESIGN MODEL— GENERAL PROCEDURE

For sections containing at least the minimum amount of transverse reinforcement specified in Article 5.7.2.5, the values of  $\beta$  and  $\theta$  shall be as specified in Table B5.2-1. In using this table,  $\epsilon_x$  shall be taken as the calculated longitudinal strain at the mid-depth of the member when the section is subjected to  $M_u$ ,  $N_u$ , and  $V_u$  as shown in Figure B5.2-1.

For sections containing less transverse reinforcement than specified in Article 5.7.2.5, the values of  $\beta$  and  $\theta$  shall be as specified in Table B5.2-2. In using this table,  $\epsilon_x$  shall be taken as the largest calculated longitudinal strain which occurs within the web of the member when the section is subjected to  $N_u$ ,  $M_u$ , and  $V_u$  as shown in Figure B5.2-2.

Where consideration of torsion is required by the provisions of Article 5.7.2,  $V_u$  in Eqs. B5.2-3 through B5.2-5 shall be replaced by  $V_{eff}$ .

For solid sections:

$$V_{eff} = \sqrt{V_u^2 + \left( \frac{0.9 p_h T_u}{2 A_o} \right)^2} \quad (\text{B5.2-1})$$

For hollow sections:

$$V_{eff} = V_u + \frac{T_u d_s}{2 A_o} \quad (\text{B5.2-2})$$

Unless more accurate calculations are made,  $\epsilon_x$  shall be determined as:

- If the section contains at least the minimum transverse reinforcement as specified in Article 5.7.2.5:

$$\epsilon_x = \frac{\left( \frac{|M_u|}{d_v} + 0.5 N_u + 0.5 |V_u - V_p| \cot \theta - A_{ps} f_{po} \right)}{2(E_s A_s + E_p A_{ps})} \quad (\text{B5.2-3})$$

### CB5.2

The shear resistance of a member may be determined by performing a detailed sectional analysis that satisfies the requirements of Article 5.7.3.1. Such an analysis (see Figure CB5.2-1) would show that the shear stresses are not uniform over the depth of the web and that the direction of the principal compressive stresses changes over the depth of the beam. The more direct procedure given herein assumes that the concrete shear stresses are uniformly distributed over an area  $b_v$  wide and  $d_v$  deep, that the direction of principal compressive stresses (defined by angle  $\theta$ ) remains constant over  $d_v$ , and that the shear strength of the section can be determined by considering the biaxial stress conditions at just one location in the web. See Figure CB5.2-2.

For solid cross-section shapes, such as a rectangle or an “I,” there is the possibility of considerable redistribution of shear stresses. To make some allowance for this favorable redistribution it is safe to use a root-mean-square approach in calculating the nominal shear stress for these cross sections, as indicated in Eq. B5.2-1. The  $0.9 p_h$  comes from 90 percent of the perimeter of the spalled concrete section. This is similar to multiplying 0.9 times the lever arm in flexural calculations.

For a hollow girder, the shear flow due to torsion is added to the shear flow due to flexure in one exterior web, and subtracted from the opposite exterior web. In the controlling web, the second term in Eq. B5.2-2 comes from integrating the distance from the centroid of the section, to the center of the shear flow path around the circumference of the section. The stress is converted to a force by multiplying by the web height measured between the shear flow paths in the top and bottom slabs, which has a value approximately equal that of  $d_s$ . If the exterior web is sloped, this distance should be divided by the sine of the web angle from horizontal.

Members containing at least the minimum amount of transverse reinforcement have a considerable capacity to redistribute shear stresses from the most highly strained portion of the cross section to the less highly strained portions. Because