Analysis and Design of Reinforced Concrete Bridge Structures

Reported by Joint ACI-ASCE Committee 343

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These recommendations, reported by Joint ACI-ASCE Committee 343 on Concrete Bridge Design, provide currently acceptable guidelines for the analysis and design of reinforced, prestressed, and partially prestressed concrete bridges based on the state of the art at the time of writing the report. The provisions recommended herein apply to pedestrian bridges, highway bridges, railroad bridges, airport taxiway bridges, and other special bridge structures. Recommendations for Transit Guideways are given in ACI 358R.

The subjects covered in these recommendations are: common terms; general considerations; materials; construction; loads and load combinations; preliminary design; ultimate load analysis and strength design; service load analysis and design; prestressed concrete; superstructure systems and elements; substructure systems and elements; precast concrete; and details of reinforcement.

The quality and testing of materials used in construction are covered by reference to the appropriate AASHTO and ASTM standard specifications. Welding of reinforcement is covered by reference to the appropriate AWS standard.

Keywords: admixtures; aggregates; anchorage (structural); beam-column frame; beams (supports); **bridges (structures)**; cements; cold weather construction; columns (supports); combined stress; composite construction (concrete and steel); composite construction (concrete to concrete); compressive strength; **concrete construction**; concretes; concrete slabs;

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construction joints; construction materials; continuity (structural); cover; curing; deep beams; deflection; earthquake-resistant structures; flexural strength; footings; formwork (construction); frames; hot weather construction; inspection; lightweight concretes; loads (forces); mixing; mixture proportioning; modulus of elasticity; moments; placing; precast concrete; prestressed concrete; prestressing steels; quality control; reinforced concrete; reinforcing steels; serviceability; shear strength; spans; specifications; splicing; strength; structural analysis; structural design; T-beams; torsion; ultimate strength method; water; welded-wire fabric.

Note: In the text, measurements in metric (SI) units in parentheses follow measurements in inch-pound units. Where applicable for equations, equations for metric (SI) units in parentheses follow equations in inch-pound units.

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Reference to this document shall not be made in contract documents. If items found in this document are desired by the Architect/Engineer to be a part of the contract documents, they shall be restated in mandatory language for incorporation by the Architect/Engineer.

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Complex highway interchange in California with 15 bridge structures

CHAPTER 1—DEFINITIONS, NOTATION, AND ORGANIZATIONS

1.1—Introduction

This chapter provides currently accepted definitions, notation, and abbreviations particular to concrete bridge design practice which have been used in the preparation of this document.

Concrete bridge types commonly in use are described separately in Chapter 2, Requirements for Bridges, in Chapter 6, Preliminary Design, and in Chapter 11, Superstructure Systems and Elements.

1.2—Definitions

For cement and concrete terminology already defined, reference is made to ACI 116R. Terms not defined in ACI 116R or defined differently from ACI 116R are defined for specific use in this document as follows:

aggregate, normal weight—aggregate with combined dry, loose weight, varying from 110 lb. to 130 lb/ft³ (approximately 1760 to 2080 kg/m³).

compressive strength of concrete (f'_c) —specified compressive strength of concrete in pounds per square inch (psi) or (MPa).

Wherever this quantity is under a radical sign, the square root of the numerical value only is intended and the resultant is in pounds per square inch (psi) or (MPa).

concrete, heavyweight—a concrete having heavyweight aggregates and weighing after hardening over 160 lb/ft^3 (approximately 2560 kg/m³).

concrete, **shrinkage-compensating**—an expansive cement concrete in which expansion, if restrained, induces

compressive strains that are intended to approximately offset tensile strains in the concrete induced by drying shrinkage.

concrete, structural lightweight—concrete containing lightweight aggregate having unit weight ranging from 90 to 115 lb/ft³ (1440 to 1850 kg/m³). In this document, a lightweight concrete without natural sand is termed "all-lightweight concrete," and lightweight concrete in which all fine aggregate consists of normal weight sand is termed "sand-lightweight concrete."

design load—applicable loads and forces or their related internal moments and forces used to proportion members. For service load analysis and design, design load refers to loads without load factors. For ultimate load analysis and strength design, design load refers to loads multiplied by appropriate load factors.

effective prestress—the stress remaining in concrete due to prestressing after all losses have occurred, excluding the effect of superimposed loads and weight of member.

load, dead—the dead weight supported by a member (without load factors).

load, **live**—the live load specified by the applicable document governing design (without load factors).

load, service—live and dead loads (without load factors). **plain reinforcement**—reinforcement without surface deformations, or one having deformations that do not conform

to the applicable requirements for deformed reinforcement. **pretensioning**—a method of prestressing in which the tendons are tensioned before the concrete is placed.

surface water—water carried by an aggregate except that held by absorption within the aggregate particles themselves.

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1.3—Notation

Preparation of notation is based on ACI 104R. Where the same notation is used for more than one term, the uncommonly used terms are referred to the Chapter in which they are used. The following notations are listed for specific use in this report:

- *a* = depth of equivalent rectangular stress block
- *a* = constant used in estimating unit structure dead load (Chapter 5)
- a = compression flange thickness (Chapter 7)
- a_b = depth of equivalent rectangular stress block for balanced conditions
- a_i = fraction of trucks with a specific gross weight
- a_v = ratio of stiffness of shearhead arm to surrounding composite slab section
- effective tension area of concrete surrounding the main tension reinforcing bars and having the same centroid as that reinforcement, divided by the number of bars, or wires. When the main reinforcement consists of several bar or wire sizes, the number of bars or wires should be computed as the total steel area divided by the area of the largest bar or wire used
- A = axial load deformations and rib shortening used in connection with *t*-loads (Chapter 5)
- A_b = area of an individual bar
- A_c = area of core of spirally reinforced compression member measured to the outside diameter of the spiral
- A_e = area of longitudinal bars required to resist torsion
- A_e = effective tension area of concrete along side face of member surrounding the crack control reinforcement (Chapter 8)
- A_f = area of reinforcement required to resist moment developed by shear on a bracket or corbel
- A_g = gross area of section
- A_h = area of shear reinforcement parallel to flexural tension reinforcement
- A_l = total area of longitudinal reinforcement to resist torsion
- A_n = area of reinforcement in bracket or corbel resisting tensile force N_{uc}
- A_{ps} = area of prestressed reinforcement in tension zone
- A_s = area of tension reinforcement
- $A_{s'}$ = area of compression reinforcement
- A_{sa} = area of bonded reinforcement in tension zone A_{se} = area of stirrups transverse to potential bursting crack and within a distance s_e
- A_{sf} = area of reinforcement to develop compressive strength of overhanging flanges of I- and Tsections
- A_{sh} = total area of hoop and supplementary cross ties in rectangular columns
- A_{st} = total area of longitudinal reinforcement (in compression members)

- A_t = area of one leg of a closed stirrup resisting torsion within a distance s
- A_{ν} = area of shear reinforcement within a distance *s*, or area of shear reinforcement perpendicular to flexural tension reinforcement within a distance *s*, for deep flexural members
- A_{vf} = area of shear-friction reinforcement
- A_{vh} = area of shear reinforcement parallel to the flexural tension reinforcement within a distance s_2
- A_w = area of an individual wire
- A_1 = loaded area, bearing directly on concrete
- A_2 = maximum area of the portion of the supporting surface that is geometrically similar to, and concentric with, the loaded area
- b = width of compressive face of member
 - = constant used in estimating unit structure dead load (Chapter 5)
- *b* = width or diameter of pier at level of ice action (Chapter 5)
 - = width of web (Chapter 6)
 - = width of section under consideration (Chapter 7)
- b_e = width of concrete section in plane of potential bursting crack
- b_o = periphery of critical section for slabs and footings
- b_v = width of the cross section being investigated for horizontal shear
- b_w = web width, or diameter of circular section
- B = buoyancy
 - distance from extreme compressive fiber to neutral axis
- C = construction, handling, and erection loads (Chapter 5)
- *C* = stiffness parameter used in connection with lateral distribution of wheel loads to multibeam precast concrete bridges (Chapter 10)
- C = ultimate creep coefficient (Chapter 5)
- C_a = indentation coefficient used in connection with ice forces
- C_e = exposure coefficient used in connection with wind forces
- C_i = coefficient for pier inclination from vertical
- C_m = factor used in determining effect of bracing on columns (Chapter 7)
- C_t = factor relating shear and torsional stress properties equal to b_w times d divided by the summation of x^2 times y
 - = creep deformation with respect to time (Chapter 5)
- C_u = ultimate creep deformation (Chapter 5)
- C_u = ultimate creep coefficient
- C_w = shape factor relating to configuration of structure and magnitude of wind force on structure
- *CF* = centifugal force
- *d* = distance from extreme compressive fiber to centroid of tension reinforcement
 - = depth of section under consideration (Chapter 7)
 - = depth of girder (Chapter 5)
 - = distance from extreme compressive fiber to

 f_f

 f_l

 f_{lc}

 f_{lf}

 f_{lp}

 f_{lr}

 f_{ls}

 f_{ps}

 f_{pu}

 f_{py}

 f_s

 f_{s}'

 f'_{sb}

 f_{se}

 f_t

 f_v

 f_{va}

 f_{yh}

F

F

 F_a

g

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centroid of compression reinforcement

- d_b = nominal diameter of bar, wire, or prestressing strand
- d_c = thickness of concrete cover measured from the extreme tensile fiber to the center of the bar located closest thereto
- d_p = effective depth of prestressing steel (Chapter 7)
- $\dot{d_s}$ = effective depth for balanced strain conditions (Chapter 7)
- d_u = effective depth used in connection with prestressed concrete members (Chapter 7)
- D = dead load
- D = diameter of lead plug in square or circular isolation bearing (Chapter 11)
- D_f = depth of footing
- DF = distribution factor used in connection with live loads
- DR = derailment force
- DS = displacement of supports
- *e* = base of Napierian logarithms
- e = span for simply supported bridge or distance between points of inflection under uniform load (Chapter 10)
- *e* = eccentricity of design load parallel to axis measured from the centroid of the section (Chapter 7)
- $e_b = M_b/P_b$ = eccentricity of the balanced conditionload moment relationship
- e_n = clear span length of slab (Chapter 10)
- e_1 = length of short span of slab
- e_2 = length of long span of slab
- *E* = effective width of concrete slab resisting wheel or other concentrated load (Chapter 10)
- E = earth pressure used in connection with loads (Chapter 5)
- E_c = modulus of elasticity of concrete
- E_{ci} = modulus of elasticity of concrete at transfer of stress
- E_{ps} = modulus of elasticity of prestressing strand
- $\vec{E_s}$ = modulus of elasticity of steel
- *EI* = flexural stiffness of compression members
- EQ = earthquake force
- f = natural frequency of vibration of structure (Chapter 5)
- f_a = axial stress
- f_a = basic allowable stress (Chapter 5)
- f_b = bending stress
- f_b = average bearing stress in concrete on loaded area (Chapter 8)
- f_c = extreme fiber compressive stress in concrete at service loads
- f'_c = specified compressive strength of concrete
- f_{cds} = change in concrete stress at center of gravity of prestressing steel due to all dead loads except the dead load acting at the time the prestressing force is applied
- f_{ci} = compressive strength of concrete at time of initial prestress

- f_{cir} = concrete stress immediately after transfer at center of gravity of prestressing steel
- f_{cp} = concrete bearing stress under anchor plate of post-tensioning tendon
- f_{ct} = average splitting tensile strength of lightweight aggregate concrete
 - = stress range

= stress produced by *i*th loading (Chapter 5)

- = loss in prestressing steel stress due to creep
- f_{le} = loss in prestressing steel stress due to elastic shortening
 - = loss in prestressing steel stress due to friction
 - = total loss in prestressing steel stress
 - = loss in prestressing steel stress due to relaxation
 - = loss in prestressing steel stress due to shrinkage
- f_{min} = algebraic minimum stress level where tension is positive and compression is negative
- f_{pc} = compressive stress in the concrete, after all prestress losses have occurred, at the centroid of the cross section resisting the applied loads or at the junction of the web and flange when the centroid lies in the flange. (In a composite member, f_{pc} will be the resultant compressive stress at the centroid of the composite section, or at the junction of the web and flange when the centroid lies within the flange, due to both prestress and to bending moments resisted by the precast member acting alone)
- f_{pe} = compressive stress in concrete due to prestress only, after all losses, at the extreme fiber of a section at which tensile stresses are caused by applied loads
- f_{po} = steel stress at jacking end of post-tensioning tendon
 - = stress in prestressing steel at design loads
 - = ultimate strength of prestressing steel
 - = specified yield strength of prestressing tendons
 - = modulus of rupture of concrete
 - = tensile stress in reinforcement at service loads
 - = stress in compressive reinforcement
 - stress in compressive reinforcement at balanced conditions
 - = effective stress in prestressing steel, after losses
 - extreme fiber tensile stress in concrete at service loads
 - = specified yield stress, or design yield stress of nonprestressed reinforcement
 - = design yield stress of steel of bearing plate
 - design yield stress of steel for hoops and supplementary cross ties in columns
 - = frictional force
 - = horizontal ice force on pier (Chapter 5)
 - = allowable compressive stress
- F_b = allowable bending stress
 - = acceleration due to gravity, 32.2 ft/sec² (9.81 m/sec²)
- G_A = ratio of stiffness of column to stiffness of members at A end resisting column bending

ANALYSIS AND DESIGN OF REINFORCED CONCRETE BRIDGE STRUCTURES (ACI 343R-95)

- G_A = degree of fixity in the foundation (Chapter 11) = ratio of stiffness of column to stiffness of G_B members at B end resisting column bending G_{avg} = average ratio of stiffness of column to stiffness of members resisting column bending = minimum ratio of stiffness of column to stiffness G_{min} of members resisting column bending h = overall thickness of member h = slab thickness (Chapter 6) = height of rolled on transverse deformation of h deformed bar (Chapter 8) h = height of fill (Chapter 5) = thickness of ice in contact with pier (Chapter 5) h = asphalt wearing surface thickness (Chapter 5) h h_a = thickness of bearing plate = core dimension of column in direction under h_c consideration = compression flange thickness of I- and T h_{f} sections = thickness of standard slab used in computing h_o shrinkage h_2 = thickness of bottom slab of box girder (Chapter 6) Η = average height of columns supporting bridge deck Η = curvature coefficient (Chapter 9) = impact due to live load (Chapter 5) I I = impact coefficient = moment of inertia (Chapter 7) I ICE = ice pressure = moment of inertia of cracked section with rein- I_{cr} forcement transformed to concrete I_e = effective moment of inertia for computation of deflection (Chapter 8) = moment of inertia of gross concrete section I_g about the centroidal axis, neglecting the reinforcement = moment of inertia of reinforcement about the I_s centroidal axis of the member cross section k = effective length factor for compression member (Chapters 7 and 11) = dimensionless coefficient for lateral distribution k of live load for T- and I-girder bridge (Chapter 10)k = coefficient for different supports in determining earthquake force (Chapter 5) = dimensionless coefficient for lateral distribution k, of live load for spread box-beam bridges (Chapter 10) = wobble friction coefficient of prestressing steel Κ (Chapter 9) K = constant used in connection with stream flow (Chapters 5 and 11)
- K = value used for beam type and deck material (Chapter 10)
- Κ = pier stiffness (Chapter 11)
- 1 = length

- l_a = additional embedment length at support or at point of inflection = distance from face of support to load for l_a brackets and corbels (Chapter 7) = basic development length for deformed bar in l_{bd} compression development length l_d = development length for deformed bars in tension l_{dh} terminating in a standard hook l_{hb} = basic development length of hooked bar = clear span measured face-to-face of supports l_n l_n = length of tendon (Chapter 3) unsupported length of compression member l_u = L = live load L = span length used in estimating unit structure dead load (Chapter 5) L = bridge length contributing to seismic forces (Chapter 5) L length of compression member used in = computing pier stiffness (Chapter 11) LF = longitudinal force from live load М = number of individual loads in the load combination considered М = live load moment per unit width of concrete deck slab (Chapter 10) M_a = maximum moment in member at stage for which deflection is being computed nominal moment strength of a section at simul- M_{h} = taneous assumed ultimate strain of concrete and yielding of tension reinforcement (balanced conditions) M_{c} = factored moment to be used for design of compression member = moment causing flexural cracking at sections M_{cr} due to externally applied loads = modified moment (Chapter 7) M_m $M_{max} =$ maximum factored moment due to externally applied loads, dead load excluded M_n nominal moment strength of section = M_{nx} = nominal moment strength of section about x-axis M_{ny} = nominal moment strength of section about y-axis M_{μ} factored moment at section, $M_{\mu} = \phi M_{\mu}$ = $M_{\mu x}$ = factored moment at section about x-axis, $M_{\mu x} = \phi$ M_{nx} $M_{\mu\nu}$ = factored moment at section about y-axis, $M_{\mu\nu} = \phi$ M_{nv} M_r = applied design moment component about *x*-axis $M_{\rm v}$ = applied design moment component about y-axis value of smaller factored end moment on M_1 = compression member calculated from a conventional or elastic analysis, positive if member is bent in single curvature, negative if bent in double curvature value of larger factored end moment on M_2 compression member calculated by elastic analysis, always positive
 - modular ratio E /E

ANALYSIS AND DESIGN OF REINFORCED CONCRETE BRIDGE STRUCTURES (ACI 343R-95)

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- *n* = number of individual loads in the load combination considered (Chapter 5)
- n_b = number of girders (Chapter 10)
- n_e = number of design traffic lanes (Chapter 10)
- N = nosing and lurching force
- N = minimum support length (Chapter 5)
- NB = number of beams
- *NL* = number of design traffic lanes
- N_u = design axial load normal to the cross section occurring simultaneously with V_u , to be taken as positive for compression, negative for tension, and to include the effects of tension due to shrinkage and creep
- N_{uc} = factored tensile force applied at top of bracket or corbel acting simultaneously with V_u , taken as positive for tension
- *o* = overhang of bridge deck beyond supporting member (Chapter 6)
- o = effective ice strength (Chapter 5)
- OL = overload
- p = allowable bearing
- p = minimum ratio of bonded reinforcement in tension zone to gross area of concrete section (Chapter 9)
- p = unit weight of air (Chapter 5)
- p = proportion of load carried by short span of twoway slab (Chapter 10)
- P = load on one rear wheel of truck equal to 12,000 lb (53.4 kN) for HS15 loading and 16,000 lb (71.1 kN) for HS20 loading (Chapter 10)
- P = load above ground (Chapter 11)
- P_b = design axial load strength of a section at simultaneous assumed ultimate strain of concrete and yielding of tension reinforcement (balanced conditions)
- P_{cr} = critical buckling load
- P_n = nominal axial load at given eccentricity
- P_{nx} = nominal axial load at given eccentricity about x-axis
- P_{ny} = nominal axial load at given eccentricity about yaxis
- P_{nxy} = nominal axial load strength with biaxial loading
- P_o = nominal load strength at zero eccentricity
- P_o = at rest earth pressures (Chapter 5)
- P_s = ratio of spiral reinforcement
- P_u = moment, shear, or axial load from the *i*th loading (Chapter 5)
- P_u = factored axial load at given eccentricity, $P_u = \phi$ P_n
- P_{ux} = factored axial load strength corresponding to M_{ux} with bending considered about the x-axis only
- P_{uy} = factored axial load strength corresponding to M_{uy} with bending considered about the y-axis only

 P_{uxy} = factored axial load strength with biaxial loading

q = dynamic wind pressure

- = radius of gyration of the cross section of compression member
- base radius of rolled on transverse deformation of deformed bar (Chapter 8)
- R = average annual ambient relative humidity, percent
- R_n = characteristic strength (moment, shear, axial load)
- RH = mean annual relative humidity, percent (Chapter 5)
 - shear or torsion reinforcement spacing in direction parallel to longitudinal reinforcement
- s = beam spacing (Chapter 6)
- s_e = spacing of bursting stirrups
- s_2 = shear or torsion reinforcement spacing in direction perpendicular to the longitudinal reinforcement or spacing of horizontal reinforcement in wall
 - = spacing of wires
 - = span length
 - = average beam spacing for distribution of live loads (Chapter 10)
- S = shrinkage and other volume changes used in connection with loads or forces to be considered in analysis and design (Chapter 5)
- S_h = vertical spacing of hoops (stirrups) with a maximum of 4 in. (Chapter 11)
- S_h = spacing of hoops and supplementary cross ties
- SF = stream flow pressure = KV^2
- SN = snow load
 - = actual time in days used in connection with shrinkage and creep (Chapter 5)
 - = age of concrete in days from loading (Chapter 5)
 - equivalent time in days used in connection with shrinkage (Chapter 5)
 - = thickness of web in rectangular box section
 - = temperature at distance y above depth of temperature variation of webs
 - = temperature reduction for asphalt concrete
 - = temperature
 - = maximum temperature at upper surface of concrete (Chapter 5)
 - = fundamental period of vibration of the structure (Chapter 5)
- T^* = minimum temperature of top slab over closed interior cells (Chapter 5)
- T_c = nominal torsional moment strength provided by concrete
- T_n = nominal torsional moment strength
- T_s = nominal torsional moment strength provided by torsional reinforcement
- T_u = factored torsional moment at section
 - = total applied design shear stress at section
 - = permissible shear stress carried by concrete
- v_{dh} = design horizontal shear stress at any cross section
 - = permissible horizontal shear stress
 - = factored shear stress at section
- V = total applied design shear force at section

α

β

 β_d

 β_1

γ

μ

μ

- V= horizontal earthquake force (Chapter 5)
- V= velocity of water used in connection with stream flow (Chapter 5)
- V= maximum probable wind velocity (Chapter 5)
- V_c = nominal shear strength provided by concrete
- = nominal shear strength provided by concrete V_{ci} when diagonal cracking results from combined shear and moment
- V_{cw} = nominal shear strength provided by concrete when diagonal cracking results from excessive principal tensile stress in web
- V_i = factored shear force at section due to externally applied loads occurring simultaneously with M_{max}
- V_n = nominal shear strength provided by concrete and shear reinforcement
- V_{nh} = nominal horizontal shear strength provided by concrete and shear reinforcement
- V_p = vertical component of effective prestress force at section considered
- V_s = nominal shear strength provided by shear reinforcement
- V_{μ} = factored shear force at section
- w = unit structure dead load
- = unit weight of concrete W_{c}
- = roadway width between curbs (Chapters 10 W_c and 11)
- = road slab width from edge of slab to midway We between exterior beam and first interior beam
- W wind load used in connection with application of = wind loads to different types of bridges
- W = total weight of structure (Chapter 5)
- W = crack width (Chapter 11)
- W_{f} = gross weight of fatigue design truck
- Ŵ, = gross weight of specific trucks used in determining fatigue design truck
- W_h wind load applied in horizontal plane =
- $\frac{W_p}{W_s}$ = weight of pier and footing below ground
- = weight of soil directly above footing
- W_{ν} = wind load applied in vertical plane
- WL = wind load applied on live load (Chapter 5)
- WL = wind load on live load
- = shorter overall dimension of rectangular part of х cross section
- = tandem spacing used in connection with aircraft х loads (Chapter 5)
- = width of box girder (Chapter 6) х
- = shorter center-to-center dimension of closed x_1 rectangular stirrup
- = distance from load to point of support (Chapter x_1 10)
- = distance from center of post to point under x_2 investigation (Chapter 10)
- = longer overall dimension of rectangular part of y cross section
- = dual spacing used in connection with aircraft y loads (Chapter 5)
- = height of box girder (Chapter 6) y

- = longer center-to-center dimension of closed rect y_1 angular stirrup
- = mean thickness of deck between webs y_d
- = distance from the centroidal axis of cross y_t section, neglecting the reinforcement, to the extreme fiber in tension
- Y_o = depth of temperature variation of webs
- Y_s = height of temperature variation in soffit slab
- = quantity limiting distribution of flexural rein-Z. forcement
- = height of top of superstructure above ground z (Chapter 5)
- = angle between inclined shear reinforcement and α longitudinal axis of member
- angle of pier inclination from vertical (Chapters α = 5 and 11)
 - = load factor used in connection with group loadings (Chapter 5)
- = total angular change of prestressing steel profile α (Chapter 9)
- = total vertical angular change of prestressing steel α_v profile (Chapter 9)
- total horizontal angular change of prestressing α_h = steel profile (Chapter 9)
- = angle between shear friction reinforcement and α_f shear plane
- = load factor for the *i*th loading (Chapter 5) α_i
- = factor used in connection with torsion reinforce- α_t ment
 - = percent of basic allowable stress (Chapter 5)
- = ratio of area of bars cut off to total area of bars at β_h section
- β_c = ratio of long side to short side of concentrated load or reaction area
 - = ratio of maximum factored dead load moment to maximum factored total load moment, always positive
 - = factor used to determine the stress block in ultimate load analysis and design
 - unit weight of soil =
- = moment magnification factor for braced frames δ_b
- δ = moment magnification factor for frames not braced against sidesway
- λ correction factor related to unit weight of = concrete
 - = coefficient of friction
 - = curvature friction coefficient (Chapter 9)
- = ductility factor (Chapter 11) μ
- = time-dependent factor for sustained loads ξ (Chapter 8)
- $(\xi_{cr})_t$ = time-dependent factor for estimating creep under sustained loads (Chapter 5)
- ξί = instantaneous strain at application of load (Chapter 5)
- $(\xi_{sh})_t$ = shrinkage at time *t* (Chapter 5)
- $(\xi_{sh})_u$ = ultimate shrinkage (Chapter 5)
- = ratio of tension reinforcement = A_s/bd ρ
- ٥' ratio of compression reinforcement = A_s'/bd

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- ρ_b = reinforcement ratio producing balanced condition
- ρ_{min} = minimum tension reinforcement ratio = A_s/bd
- $\rho_p = \text{ratio of prestressed reinforcement} = A_{ps}/bd$
- ρ_s = ratio of volume of spiral reinforcement to total volume of core (out-to-out of spirals) of a spirally reinforced compression member
- $\rho_v = (A_s + A_h)/bd$
- ρ_w = reinforcement ratio = $A_s/b_w d$
- σ = moment magnification factor for compression members
- σ = effective ice strength (Chapter 5)
- τ_f = factor used in connection with prestressed concrete member design (Chapter 7)
- ϕ = strength-reduction factor
- ϕ = angle of internal friction (Chapter 5)

1.4—Referenced organizations

This report refers to many organizations which are responsible for developing standards and recommendations for concrete bridges. These organizations are commonly referred to by acronyms. Following is a listing of these organizations, their acronyms, full titles, and mailing addresses:

AASHTO

American Association of State Highway and Transportation Officials 444 N. Capital Street, NW, Suite 225 Washington, DC 20001

ACI

American Concrete Institute PO Box 9094 Farmington Hills, MI 48333-9094

ANSI

American National Standards Institute 1439 Broadway New York, NY 10018

AREA

American Railway Engineering Association 50 F Street, NW Washington, DC 20001

ARTBA

American Road and Transportation Builders Association 525 School Street, SW Washington, DC 20024

ASCE

American Society of Civil Engineers 345 E. 47th Street New York, NY 10017

ASTM

ASTM International 100 Barr Harbor Dr. West Conshohocken, PA 19<u>428</u>

AWS

American Welding Society 550 NW LeJeune Road PO Box 351040 Miami, FL 33135

BPR

Bureau of Public Roads This agency has been succeeded by the Federal Highway Administration

CEB

Comite European du Beton (European Concrete Committee) EPFL, Case Postale 88 CH 1015 Lausanne Switzerland

CRSI

Concrete Reinforcing Steel Institute 933 N. Plum Grove Road Schaumburg, IL 60195

CSA

Canadian Standards Association 178 Rexdale Boulevard Rexdale (Toronto), Ontario Canada M9W 1R3

FAA

Federal Aviation Administration 800 Independence Avenue, SW Washington, DC 20591

FHWA

Federal Highway Administration 400 Seventh Street, SW Washington, DC 20590

GSA

General Services Administration 18 F Street Washington, DC 20405

HRB

Highway Research Board This board has been succeeded by the Transportation Research Board

PCA

Portland Cement Association 5420 Old Orchard Road Skokie, IL 60077

PCI

Precast/Prestressed Concrete Institute 209 W. Jackson Blvd. Chicago, IL 60606-6938