Table 3 — FRCEFR compositions (per concrete cubic meter)

C ⁽¹⁾	W	SP ⁽²⁾	LF	FS	CS	CA_1	CA_2	SF
[kg]	[kg]	[kg]	[kg]	[kg]	[kg]	[kg]	[kg]	[kg]
300.2	228.0	127.7	7.0	533.6	457.6	295.0	294.3	60.0

(1) - Type I 42.5R and type I 52.5R; (2) – SP - Sika ViscoCrete® 3002 HE; 1 kg = 2.2 lbs

Table 4 — Concrete compositions of the tunnel segments (per m.)										
	C	W	$SP^{(1)}$	LF	FS	CS	CA_1	CA_2	SF	PF
	[Kg]	[Kg]	[Kg]	[Kg]	[Kg]	[Kg]	[kg]	[Kg]	[kg]	[ĸg]
Specimen 1	205	165	5.44	-	580.0	220.0	530.0	540.0	-	-
Specimen 2					550.5	451.8	289.7	289.4	75	
Specimen 3	360	114	8.51	247	524.5	460.3	297.3	297.1	45	2
Specimen 4					533.6	457.6	294.5	294.3	60	

Table 4 — Concrete compositions of the tunnel segments (per m³)

(1) - Sika ViscoCrete® 3002 HE; 1 kg = 2.2 lbs

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Figure 1 — Influence of the content of PP fibers on the relative residual compressive strength; specimens subjected to 750 °C [1 MPa = 146 psi; 1 kg/m³ = 0.062 lb/ft³]



Figure 2 — Heating rate profiles used to a) select the nonmetallic fiber type; b) evaluate the compression and flexural behavior of FRCEFR (straight line – planned heating rate profile; dot line – real heating rate profile) [°F = °C x 1.8 + 32]



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Figure 4 — Influence of the level of temperature exposure on the Young's modulus [°F = °C x 1.8 + 32]

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Figure 6 — Influence of the level of temperature exposure on the flexural behavior [°F = °C x 1.8 + 32; 1 MPa = 146 psi; 1 mm = 0.0394 in]



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