222 Azizinamini and Saatcioglu REFERENCES

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HSC in Seismic Regions 223

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| | | | Vertical reinforcement | | | Т | Transverse reinforcement | | | | | |
|--------------------------|---|---|------------------------|--------------------------------------|---------|-----------------|--------------------------|--------------------------------------|------------------|-------------------------------|----------------------|---------------------|
| Specimen designation* | Applied axial load | Concrete compressive strength, psi | Bars | Nominal yield strength, ksi | Percent | Detail type† | Bar size | Nominal yield strength, ksi | Spacing, in.‡ | Area ash, in. ² | Percent [§] | Percent of ACI** |
| D60-7-4-2%-0.2P | 0.2 <i>P</i> ₀ ^{tt} | 77901‡ | 8 - #6 | 60 | 2.44 | 1 | #4 | 60 | 2% | 0.4 | 2.73 | 142 |
| D60-7-3C-1%-0.2P | 0.2 P ₀ | 737011 | 8 - #6 | 60 | 2.44 | 2 | #3 | 60 | 1% | 0.33 | 3.82 | 150 |
| D60-15-4-2%-0.2P | $0.2 P_0$ | 14,620‡‡ | 8 - #6 | 60 | 2.44 | 1 | #4 | 60 | 2% | 0.4 | 2.73 | 69 |
| D60-15-3C-1%-0.2P | 0.2 P ₀ | 14,540†‡ | 8 - #6 | 60 | 2.44 | 2 | #3 | 60 | 1% | 0.33 | 3.82 | 76 |
| D120-15-3C-2%-0.2P | 0.2 P ₀ | 14,730## | 8 - #6 | 60 | 2.44 | 2 | #3 | 120 | 2% | 0.33 | 2.36 | 107 |
| D120-15-3C-1%-0.2P | $0.2 P_0$ | 14,750## | 8 - #6 | 60 | 2.44 | 2 | #3 | 120 | 1% | 0.33 | 3.82 | 150 |
| D60-4-3C-2%-0.2P | $0.2 P_0$ | 381035 | 8 - #6 | 60 | 2.44 | 2 | #3 | 60 | 2% | 0.33 | 2.36 | 180 |
| D60-4-3C-2%-0.4P | $0.4 P_0$ | 391055 | 8 - #6 | 60 | 2.44 | 2 | #3 | 60 | 2% | 0.33 | 2.36 | 180 |
| D60-15-3C-1%-0.3P | 0.3 Po | 15,050 | 8 - #6 | 60 | 2.44 | 2 | #3 | 60 | 1% | 0.33 | 3.82 | 74 |

TABLE 1-DETAILS OF TEST SPECIMENS

*Specimen designation: DA-B-C-D-E, where A = nominal yield strength of transverse reinforcement; B = nominal compressive strength of concrete;

C = 4- #4 peripheral ties = 3C-#3 peripheral ties and #3 cross ties; D = spacing of transverse reinforcement over critical region; E = level of applied axial load. +See Fig. 4 for description of each detail type.

\$\$ Spacing of transverse reinforcement in potential plastic hinge region of test columns (see Fig. 3).

SRatio of volume of transverse reinforcement over spacing S to core volume of concrete confined by transverse reinforcement (measure out-to-out).

**Ratio of area of transverse reinforcement provided over that required by seismic provisions of ACI 318-89.

 $\dagger \dagger P_0$ is column axial load capacity, defined as follows: $P_0 = 0.85 f'_c (A_g - A_u) + A_u f_y$, where f'_c is concrete compressive strength at time of testing, ksi; A_g is gross area of column cross section, in.²; A_u is total area of logitudinal steel, in.², and f_y is yield strength of logitudinal steel obtained from coupon tests, ksi.

‡‡Concrete compressive strength at time of testing based on average of three 4 x 8-in. cylinder compression tests.

§§Concrete compressive strength at time of testing based on average of three 4 x 8-in. cylinder compression tests.

| Test | M _{MAX} experimental, inkips | M _{ACI} inkips | M _{REV} inkips | <u>М_{мах}</u> <u>М</u> асі | $\frac{M_{MAX}}{M_{REV}}$ |
|--------------------------------|---|----------------------------|----------------------------|--|---------------------------|
| D60-7-4-2 ⁵ /8-0.2P | 2195 | 1762 | · | 1.25 | _ |
| D60-7-3C-15/8-0.2P | 2104 | 1714 | — | 1.23 | _ |
| D60-15-4-2⁵⁄8-0.2P | 2402 | 2588 | 2300 | 0.93 | 1.04 |
| D60-15-3C-1%-0.2P | 2612 | 2577 | 2291 | 1.01 | 1.14 |
| D120-15-3C-25/8-0.2P | 3362 | 2600 | 2312 | 0.91 | 1.02 |
| D120-15-3C-1%-0.2P | 2550 | 2602 | 2313 | 0.98 | 1.1 |
| D60-4-3C-25%-0.2P | 1533 | 1275 | _ | 1.2 | — |
| D60-4-3C-25/8-0.4P | 1489 | 1375 | | 1.08 | |
| D60-15-3C-15/8-0.3P | 2691 | 3104 | 2395 | 0.87 | 1.12 |

TABLE 2 - MAXIMUM MEASURED AND CALCULATED MOMENT CAPACITIES

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| Column | f´ _c , MPa | $P/(A_g f_c),$ percent | Drift, percent |
|--------|-----------------------|---------------------------|-------------------|
| C168 | 85 | 28 | 3.8 |
| C173 | 85 | 51 | 2.0 |
| C167 | 67 | 31 | 4.0 |
| C171 | 67 | 57 | 1.4 |
| C163 | 86 | 63 | 1.2 |
| C165 | 116 | 42 | 2.0 |
| C164 | 86 | 63 | 4.4 |
| C166 | 116 | 42 | 4.8 |
| C175 | 91 | 35 | 3.0 |
| C177 | 91 | 52 | 1.6 |

TABLE 3-EFFECT OF AXIAL COMPRESSION ON DUCTILITY AND DRIFT RATES

Note: v and f'_c are in MPa.

| Group No. | Test | f´ _c , psi | Transverse reinforcement, percent-ACI | Δ _{MAX,} in. | Maximum drift index, percent |
|--------------|---------------------|--------------------------|---|--------------------------|---------------------------------|
| | D60-7-4-25/8-0.2P | 7790 | 142 | 1.4 | 3.9 |
| 1 | D60-15-4-25/8-0.2P | 14,620 | 69 | 1.04 | 2.9 |
| | D60-7-3C-15%-0.2P | 7370 | 150 | 1.84 | 5.1 |
| 2 | D60-15-3C-15/8-0.2P | 14,540 | 76 | 1.44 | 4.0 |

TABLE 4-EFFECT OF CONCRETE COMPRESSIVE STRENGTH

TABLE 5-EFFECT OF YIELD STRENGTH

| Test | f´ _c , psi | Yield strength, ksi | Δ _{MAX.} in. | Maximum drift index, percent | Percent of ACI |
|----------------------|--------------------------|------------------------|--------------------------|---------------------------------|----------------|
| D60-15-3C-15/8-0.2P | 14,540 | 60 | 1.44 | 4.0 | 76 |
| D120-15-3C-15/8-0.2P | 14,750 | 120 | 1.40 | 3.9 | 150 |
| D120-15-3C-25/8-0.2P | 14,730 | 120 | 1.84 | 2.8 | 107 |

| Column | f´ "MPa | $P/(A_g f'_c),$ percent | ρ _s . percent | $f_{_{yt}}$,MPa | $\rho_s f_{y_l} f/f_c$ | Drift, percent |
|--------|---------|----------------------------|-----------------------------|------------------|------------------------|-------------------|
| C163 | 86 | 63 | 4.37 | 328 | 0.17 | 1.2 |
| C164 | 86 | 63 | 4.37 | 792 | 0.40 | 4.4 |
| C165 | 116 | 42 | 4.37 | 328 | 0.12 | 2.0 |
| C166 | 116 | 42 | 4.37 | 792 | 0.30 | 4.8 |
| C170 | 67 | 57 | 2.60 | 316 | 0.12 | 1.0 |
| C171 | 67 | 57 | 2.25 | 833 | 0.28 | 1.4 |
| C172 | 67 | 57 | 2.08 | 1362 | 0.42 | 2.0 |
| C178 | 100 | 35 | 1.82 | 744 | 0.14 | 1.0 |
| C180 | 100 | 35 | 1.55 | 344 | 0.05 | 1.0 |
| C181 | 100 | 35 | 1.28 | 1126 | 0.14 | 2.0 |

TABLE 6-EFFECT OF STEEL YIELD STRENGTH F_{vt} ON DUCTILITY AND DRIFT RATIOS (4)

Note: v and f'_c are in MPa.



Fig. 1—Colums with different concrete strengths showing similar axial strain ductility ratios (adapted from Reference 4)



Fig. 2-Effect of transverse reinforcement yield strength (adapted from Reference 9)



Fig. 3-Overall view of test specimens



Fig. 4—Details of transverse reinforcement (a) Type I, single peripheral hoops; (b) Type II, peripheral hoops and cross ties