EXAMPLES

Conductor Loads $W_i = 1.24(d + I_z)I_z = 1.24(1.165 + 0.25)0.25 = 0.439 \text{ lbs/ft}$ (Eq. 2-16) $d_i = 2(0.25) + 1.165 = 1.665 \text{ in.}$ $V_l = 1,800(1.075 + 0.439)(1.5) + 200(1.5) = 4,388 \text{ lbs} = 4.4 \text{ kips}$ $T = 4(1.665/12)(1,500)(2.5) + 8,800 \sin(5/2)(2)(1.65) = 3,348 \text{ lbs}$ = 3.3 kips

Wind on Structure *Transverse Wind Loads* Wind pressure = 4(2.5) = 10 psfAreas are provided in the *Wind* loading case. The NESC force coefficient is 3.2. $W_1 = 10(3.2)(34) = 1,088 \text{ lbs} = 1.1 \text{ kips}$ $W_2 = 10(3.2)(33) = 1,056 \text{ lbs} = 1.1 \text{ kips}$ $W_3 = 10(3.2)(62) = 1,984 \text{ lbs} = 2.0 \text{ kips}$

Construction and Maintenance, Chapter 3, Section 3.1

Wind on Wires Wind pressure = 3 psf

Ground-Wire Loads The pulling slope is 3 horizontal to 1 vertical. $V_l = 1.5(1,751)(1/3) + 0.262(1,800)(1.5)/2 + 50(1.5)$ = 1,304 lbs = 1.3 kips (Alt. A controls) $V_l = 0.262(1,800)(2) + 50(2) = 1,043$ lbs = 1.1 kips (Alt. B controls) $T = 3(0.385/12)(1,500)1.5 + 1751 \sin(5/2)(2)1.5 = 446$ lbs = 0.5 kips

Conductor Loads $V_l = 1.5(5,961)(1/3) + 1.075(1,800)(1.5)/2 + 200(1.5)$ = 4,732 lbs = 4.7 kips (Alt. A controls) $V_l = 1.075(1,800)2 + 200(2) = 4,270$ lbs = 4.3 kips (Alt. B controls) $T = 3(1.165/12)(1,500)1.5 + 5,961 \sin(5/2)(2)1.5 = 1,435$ lbs = 1.4 kips

Wind on Structure *Transverse Wind Loads* Wind pressure = 3(1.5) = 4.5 psf Force coefficients and areas are provided in the *Wind* loading case. $W_1 = 4.5(1.8)(34) = 275$ lbs = 0.3 kips $W_2 = 4.5(3.22)(33) = 478$ lbs = 0.5 kips $W_3 = 4.5(3.32)(62) = 926$ lbs = 0.9 kips

Failure Containment, Chapter 3, Section 3.3.2

This loading case is based on the residual static load of a broken conductor or ground wire (0 psf wind and 0 in. of radial ice at 30°F).

Ground-Wire Loads The RSL load factor for a broken ground wire is 1.0.

Broken Wire $V_l = 0.262(1,800)/2 + 50 = 286$ lbs = 0.3 kips $T = 1,623 \sin(5/2)(1.0) = 71$ lbs = 0.1 kips $L = 1,623 \cos(5/2)(1.0) = 1,621$ lbs = 1.6 kips

Intact Wire $V_l = 0.262(1,800) + 50 = 522$ lbs = 0.5 kips $T = 1,623 \sin(5/2)(2) = 142$ lbs = 0.1 kips L = 0.0 kips

Conductor Loads Ratio of the span to insulator length = 1,250/6 = 208Ratio of the span to sag = 1,250/31.6 = 40From Fig. 3-2 in Chapter 3, the RSL load factor is 0.7. Refer to Table 5-2.

Broken Wire $V_l = 1.075(1,800)/2 + 200 = 1,168$ lbs = 1.2 kips $T = 5,615 \sin(5/2)(0.7) = 171$ lbs = 0.2 kips $L = 5,615 \cos(5/2)(0.7) = 3,927$ lbs = 3.9 kips

Intact Wire $V_l = 1.075(1,800) + 200 = 2,135$ lbs = 2.2 kips $T = 5,615 \sin(5/2)(2) = 490$ lbs = 0.5 kips L = 0.0 kips

5.1 WEIGHT SPAN CHANGE WITH BLOW-OUT ON INCLINED SPANS

This example compares weight spans with and without wind for the center tower shown in Fig. 5-2. The equations are shown in Section 4.5.1.1 of Chapter 4. Wire data is from Section 5.0 above.

Ground Wire No Wind $C_v = H/w_v = 1,546/0.262 = 5,901 \text{ ft}$ Eq. 4-7) $X_1 = S/2 - C_v \sinh^{-1}[(B/2)/C_v \sinh(S/2C_v)]$ $= 1,250/2 - 5,901 \sinh^{-1}[(50/2)/5,901 \sinh(1,250/2(5,901))]$ = 390 ft (Eq. 4-5) Weight span = 2(1,250 - 390) = 1,720 \text{ ft}



Figure 5-2. Weight span for center tower with inclined spans.

16.3-psf Wind $C_v = 2,939/0.262 = 11,218 \text{ ft}$ (Eq. 4-7) $X_1 = 1,250/2 - 1,1218 \sinh^{-1}[(50/2)/11,218 \sinh(1,250/2(11,218))]$ = 177 ft (Eq. 4-5) Weight span = 2(1,250 - 177) = 2,146 \text{ ft} (25\% increase) Conductor

No Wind $C_v = 5,302/1.075 = 4,932 \text{ ft}$ $X_1 = 1,250/2 - 4,932 \sinh^{-1}[(50/2)/4,932 \sinh(1,250/2(4,932))] = 428 \text{ ft}$ Weight span = 2(1,250 - 428) = 1,644 ft

16.3-psf Wind $C_v = 8,598/1.075 = 7,998$ ft $X_1 = 1,250/2 - 7,998 \sinh^{-1}[(50/2)/7,998 \sinh(1,250/2(7,998))] = 306$ ft Weight span = 2(1,250 - 306) = 1,888 ft (15% increase)

5.2 TRADITIONAL CATENARY CONSTANT

This example compares weight spans to those in Section 5.1 using the traditional catenary constant. The traditional catenary constant is based on the resultant unit weight (w_r). The catenary constant in Section 5.1 is based on the vertical unit weight (w_v). Figure 5-2 shows the upper and lower towers and spans.

Ground Wire
16.3-psf Wind

$$w_v = 0.262 \text{ lbs/ft}$$

 $w_r = (0.262^2 + 0.523^2)^{1/2} = 0.585 \text{ lbs/ft}$
 $C_r = H/w_r = 2,939/0.585 = 5,025 \text{ ft}$ (Eq. 4-6)
 $X_1 = S/2 - C_r \sinh^{-1}[(B/2)/C_r \sinh(S/2C_r)]$
 $= 1,250/2 - 5,025 \sinh^{-1}[(50/2)/5,025 \sinh(1,250/2(5,025))]$
 $= 425 \text{ ft}$ (Eq. 4-5)
Weight span = 2(1,250 - 425) = 1,650 \text{ ft}
Conductor
Refer to Table 5-3.
16.3-psf Wind
 $w_v = 1.075 \text{ lbs/ft}$
 $w_t = 16.3(1.165/12) = 1.582 \text{ lbs/ft}$
 $w_r = (1.075^2 + 1.582)^{1/2} = 1.913 \text{ lbs/ft}$
 $C_r = 8,598/1.913 = 4,494 \text{ ft}$ (Eq. 4-6)
 $X_1 = 1,250/2 - 4,494 \sinh^{-1}[(50/2)/4,494 \sinh(1,250/2(4,494))]$
 $= 446 \text{ ft}$ (Eq. 4-5)
Weight span = 2(1,250 - 446) = 1,608 \text{ ft}

The traditional catenary constant underestimates the vertical load on the upper tower and overestimates the vertical load on the lower tower.

APPENDIX A

DEFINITIONS, NOTATIONS, AND SI CONVERSION FACTORS

A.1 DEFINITION OF STRUCTURE TYPES

Tangent Structure: Minimum line deflection angle. Usually suspension or some type of post insulators (line post, braced line post, horizontal V) used to support the conductors and transfer wind and weight loads to the structure. In practice, structures with very small line angles, such as 2 degrees or less, are often referred to as tangent structures.

Angle Structure (change in direction in plan view):

- a. May be similar to tangent structure, using suspension or post insulators to support the conductors and transfer wind, weight, and line angle loads to the structure.
- b. May be similar to strain or dead-end structures, using insulators in series with the conductors to bring wind, weight, and line angle loads directly into the structure.

Strain Structure (usually has line angle, also): Similar to dead-end structure, using insulators in series with the conductors to bring wind, weight, and line angle loads directly into the structure. Also capable of resisting some unbalanced tensions in one direction of one or all wires on one face of the structure, but not capable of resisting the full unbalanced tensions of all wires removed on one face of the structure (i.e., with all ahead span or back span wires removed).

Dead-End Structure (usually has line angle, also): Uses insulators in series with the conductors to bring wind, weight, and line angle loads directly into the structure. Also (generally) capable of resisting the full

unbalanced tensions of all wires removed on one face of the structure (i.e., with ahead span or back span wires removed).

A.2 DEFINITIONS OF SPAN

Span. The distance, generally measured horizontally, between two points. Unless otherwise stated, span usually refers to the distance between two adjacent structures. See Fig. A-1.

Span Length. The horizontal distance between two adjacent structures.

Back Span. The span length in the span behind (generally in the direction of decreasing stationing) the structure in question. In Fig. B-1, span 1 is the back span of structure B.

Ahead Span. The span length in the span ahead (generally in the direction of increasing stationing) of the structure in question. In Fig. B-1, span 2 is the fore span (ahead span) of structure B.

Sag. The relative vertical distance of the straight line made by two adjacent supports to a point along a conductor.

Slack. The amount of conductor length difference between a straight line made by two adjacent supports and a sagging conductor.



Figure A-1. Span usually refers to the distance between two adjacent structures.

APPENDIX A

Weight Span. The horizontal distance between the low point of sag in back span and the low point of sag in the ahead span. It is used in calculating the vertical load that the conductor imposes on the supporting structure.

Wind Span. The mathematical average of the back span and the fore span. It is used in calculating the wind load that the conductor imposes on the supporting structure. This may also be referred to as the horizontal span.

Vertical Span. The vertical span is the same as the weight span.

A.3 NOTATION

The following notation is used in this manual:

- *A* solid tributary area of surfaces projected normal to the wind, in square feet
- *A*_i cross-sectional area of ice accretion on a wire, in inches
- $A_{\rm m}$ the area of all members in the windward face of a structure, in square feet
- $A_{\rm ml}$ the area of all members in the face of the structure that, in a tangent structure, is parallel to the line, in square feet
- $A_{\rm mt}$ the area of all members in the face of the structure that, in a tangent structure, is perpendicular to the line, in square feet
- A_{o} the area of the outline of the windward face of a structure, in square feet
- *B* difference in elevation of supports, in feet
- *B*_t dimensionless response term corresponding to the quasi-static background wind loading on the structure
- $B_{\rm w}$ dimensionless response term corresponding to the quasi-static background wind loading on the wire (conductor or ground wire)
- BWL broken wire load

c correction factor for aspect ratio

- C catenary constant or parameter of the catenary curve
- *C*_f force coefficient
- $C_{\rm fl}$ the force coefficient associated with faces of the structure that, in a tangent structure, are parallel to the line
- $C_{\rm ft}$ the force coefficient associated with faces of the structure that, in a tangent structure, are perpendicular to the line
- C&M construction and maintenance loads
- COV_{R} coefficient of variation of component strength
- *d* diameter of wire (conductor or ground wire), in inches
- *D* straight-line distance between the supports, in feet

96 ELECTRICAL TRANSMISSION LINE STRUCTURAL LOADING

- DL dead loads from weights of components
- *e* exclusion limit of component strength, in percentage
- *E* exposure factor evaluated at the effective height of the wire or structure
- *f* structure/member natural frequency, in cycles/second
- $f_{\rm t}$ fundamental frequency of the free-standing structure in the transverse direction, in Hertz
- $f_{\rm w}$ fundamental frequency for horizontal sway of the conductor or ground wire, in Hertz
- *F* wind force, in pounds or kips (1,000 pounds)
- F_1 wind force in the longitudinal direction, in pounds or kips
- $F_{\rm t}$ wind force in the transverse direction, in pounds or kips
- FC failure containment loads
- FPP Fujita-Pearson tornado scale
- G gust response factor
- $g_{\rm s}$ statistical peak factor for gust response of a component
- $G_{\rm t}$ gust response factor for the structure
- $G_{\rm w}$ gust response factor for the wire (conductor or ground wire)
- *H* height of hill or escarpment relative to the upwind terrain, in feet
- *HA* horizontal line angle, in degrees
- I_{RP} ice thickness having an RP-year return period, in inches
- I_{50} ice thickness having a 50-year return period, in inches
- I_Z design ice thickness, in inches
- *K*₁ factor to account for shape of topographic feature and maximum speed-up effect
- *K*₂ factor to account for reduction in speed-up with distance upwind of downwind effect
- K_3 factor to account for reduction in speed-up with height above local terrain
- K_v ratio of the 3-sec wind speed to the 10-min average wind speed in open country (Exposure C) at 33-ft (10-m) reference height
- *K*_Z velocity pressure exposure coefficient
- *K*_{zt} topographic factor
- LEL lower exclusion limit
- LL legislated loads
- *L*_h distance upwind of crest to where the difference in ground elevation is half the height of hill or escarpment, in feet
- $L_{\rm m}$ length of member, in feet
- *L*_s transverse integral scale of turbulence, in feet
- $L_{\rm T}$ transverse structure load, in pounds or kips
- $L_{\rm V}$ vertical structure load, in pounds or kips
- $m_{\rm i}$ mass of typical ice sample
- PDF probability density function of a random variable

APPENDIX A

$P_{\rm f}$	component annual probability of failure
0	the numerical constant determined by air density
$\tilde{O}_{\rm D}$	design load effect in each component of a structure
$\tilde{O}_{\rm RP}$	weather-related load with an RP-vear return period
\widetilde{O}_{50}	weather-related load with a 50-year return period
\tilde{R}^{30}	Revnolds number
R.	nominal value of component strength
R.	dimensionless resonant response term of the structure
R	dimensionless resonant response term of the wire
RP	return period of weather-related event load or load effect
RRE	relative reliability factor
RSI	residual static load for the broken wire loading condition
PTC	rated tension strongth
KI3	member diameter or width normal to the wind in feet
5 C	appendent of the using (conductor and ground using) in fact
5 C 1	Span length of the whes (conductor and ground whe), in feet
501 1	time
l T	unter harizantal component of tancian in nounda ar line
1 _H	horizontal component of tension, in pounds of kips
ип	norizontal component of unit wire load for a certain tension, in
מוו	pounds or kips
	resultant unit wire load for a certain tension, in pounds or kips
uv	vertical component of unit wire load for a certain tension, in
17	design swind encode (2 cost) at standard beight of 22 ft (10 m) in
V	design wind speed (5-sec) at standard height of 55 ht (10 ht) in
17	open country (Exposure C), in miles per nour (mpn)
V 50	wind speed at a 50-year return period (basic wind speed), 3-sec
T.7	gust, in mpn
V _{cr}	critical vortex-induced wind speed, in feet per second
V_l	vertical structure load, in pounds or kips
V _o	10-min average wind speed at the effective height of the wires
T 7	and structure, in ft/sec
$V_{\rm RP}$	wind velocity having an RP-year return period, 3-sec gust, in
T 7 4	mph
VA	vertical line angle, in degrees
W	wire weight per unit length, in pounds per foot
W1	weight of glaze ice, in pounds per foot
X_1	distance from the low point of sag to lower support, in feet
Z	height above ground, in feet
z_{g}	gradient height, in feet
$z_{\rm h}$	effective height above ground of the wire (conductor or ground
	wire) or structure, in feet
α	power-law coefficient for terrain factor equation
α_{FM}	power-law coefficient for sustained wind
γ	load factor applied to weather-related loads Q_{50}

98 ELECTRICAL TRANSMISSION LINE STRUCTURAL LOADING

- γ_{CM} load factor applied to construction and maintenance loads
- γ_i load factor applied to ice load
- γ_w load factor applied to wind load
- ε approximate coefficient for separation of the wire and structure response terms in the general gust response factor equations
- κ surface drag coefficient
- ρ mass density of air
- ρ_i ice density
- Φ the solidity ratio ($A_{\rm m}/A_{\rm o}$)
- ϕ_{LL} strength factor specified with legislated loads
- ζ_t structure damping to critical damping ratio
- ζ_{w} wire aerodynamic damping to critical damping ratio
- Ψ angle of yaw, in degrees

A.4 SI CONVERSION FACTORS

- 1 ft = 0.305 meter (m)
- 1 in. = 25.4 millimeters (mm)
- 1 pound (lb) force = 4.45 newtons (N)
- 1 lb/ft = 14.6 N/m
- $1 \text{ lb/ft}^2 \text{ (psf)} = 47.8 \text{ pascals (Pa) (N/m}^2)$
- 1 lb mass/ft³ (pcf) = 0.016 gram/cubic centimeter (g/c^3)
- 1 mile per hour (mph) = 0.45 meter/second (m/s)
- To convert temperature, θ , from °F to °C, θ (°C) = 5/9 [θ (°F) 32°F]