- (7) A sequence of fine layers with greatly differing composition and/or mechanical properties may be considered as one stratum if the overall behaviour is relevant, and the behaviour can be adequately represented by ground parameters selected for the stratum.
- (8) When deriving the boundary between different ground layers and the groundwater level, there may be interpolated linearly between the investigation points provided the spacing is sufficiently small and the geological conditions are sufficiently homogeneous. Such application of linear interpolations and their justification should be reported.

6.4 Establishment of derived values

(1)P If correlations have been used to derive geotechnical parameters or coefficients, the correlations and their applicability shall be documented.

Annex A

(Informative)

List of test results of geotechnical test standards

(1) In Table A.1, field and laboratory tests are listed together with the respective test results which should be presented in the Ground Investigation Report (if applicable).

Table A.1 — List of test results of geotechnical standards

Field test ^a	Test results	
CPT	 Cone penetration resistance (q_c) 	
	 Local unit side friction (f_s) 	
	- Friction ratio $(R_{\rm f})$	
CPTU	 Corrected cone resistance (q_t) 	
	 Local unit side friction (f_s) 	
	 Measured pore pressure (u) 	
Dynamic probing	 Number of blows N₁₀ for the following tests: DPL, DPM, DPH 	
	- Number of blows (N_{10}) or (N_{20}) for the DPSH test	
SPT	 Number of blows N 	
	- Energy correction $E_{\rm r}$	
	 Soil description 	
Ménard pressuremeter test	- Pressuremeter modulus $(E_{\rm M})$	
	- Creep pressure $(p_{\rm f})$	
	- Limit pressure (p_{LM})	
	 Expansion curve 	
Flexible dilatometer test	- Dilatometer modulus ($E_{\rm FDT}$)	
	 Deformation curve 	
All other pressuremeter tests	 Expansion curve 	
Field vane test	– Undrained shear strength (uncorrected) ($c_{ m fv)}$	
	- Remoulded undrained shear strength (c_{rv})	
	 Torque-rotation curve 	
Weight sounding test	 Continuous record of weight sounding resistance 	
	 Weight sounding resistance is: 	
	 either the penetration depth for a standard load; 	
	 or the number of half-turns required for every 	
	0,2 m penetration, at the standard load of 1 kN	
Plate loading test	 Ultimate contact pressure (p_u) 	
Flat dilatometer test	- Corrected lift-off pressure (p_0)	
	- Corrected expansion pressure (p_1) at 1,1 mm	
	- Dilatometer modulus E_{DMT} , material index (I_{DMT})	
	and horizontal stress index (K_{DMT})	

Table A.1 (continued)

Laboratory test ^b	Test results			
Water content (soil)	- Value of (w)			
Bulk mass density (soil)	– Value of (ρ)			
Particle mass density (soil)	- Value of (ρ_s)			
Particle size distribution	 Grain size distribution curve 			
(soil)				
Consistency limits (soil) Density index (soil)	- Plastic and liquid limit values (w_P) , (w_L)			
Organic content (soil)	- Values of e_{max} , e_{min} and I_{D} - AC1) Loss on ignition (AC1) (C_{OM})			
Carbonate content (soil)				
Sulfate content (soil)	 Value of carbonate content (C_{CaCO3}) Value of sulfate content (C_{SO4}²⁻) or (C_{SO3}²⁻) 			
Chlorite content (soil)	 Value of sulface content (C_{S04}) of (C_{S03}) Value of chlorite content (C_{Cl}) 			
pH (soil)	- Value of pH			
Compressibility oedometer	 Compressibility curve (different options) 			
(soil)	 Consolidation curves (different options) 			
	 Secondary compression curve (creep curve) 			
	- Values of E_{oed} (stress interval) and σ_p or C_s , C_c , σ_p			
	- Value of C_{α}			
Laboratory vane (soil)	 Value of strength index (c_u) 			
Fall cone (soil)	 Value of strength index (c_u) 			
Unconfined compression (soil)	- Value of strength index $q_u = 2c_u$			
Unconsolidated undrained compression (soil)	- Value of undrained shear strength $(c_{\rm u})$			
Consolidated triaxial	Stress-strain curve(s) and pore pressure curve			
compression (soil)	Stress paths			
	- Mohr circles			
	$-c', \varphi'$ or $c_{\rm u}$			
	- Variations of $c_{\rm u}$ with $\sigma_{\rm c}$			
	- Deformation parameter(s) (E') or (E_u)			
Consolidated direct shear	 Stress-displacement curve 			
box (soil)	$ \tau$ – σ diagram			
	- c', φ'			
	 Residual parameters 			

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Table A.1 (continued)

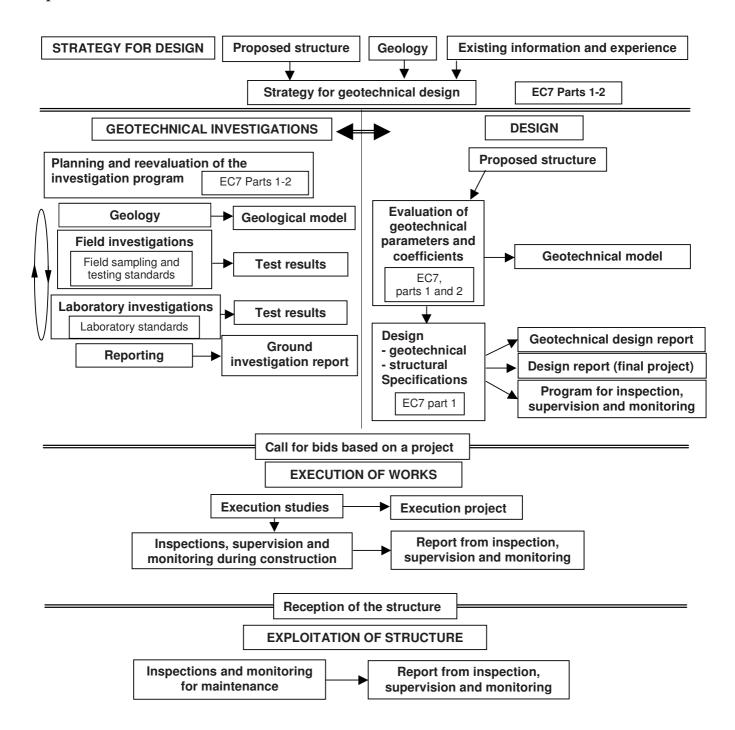
Laboratory test b	Test results
California bearing ratio (soil)	- Value of the CBR index (<i>I</i> _{CBR})
Permeability (soil)	 Value of the coefficient of permeability (k):
	 from direct laboratory permeability test
	 from field permeability tests
	 from oedometer test
Water content (rock)	- Value of w
Density and porosity (rock)	- Value of ρ and n
Swelling (rock)	Swelling Strain Index
	 Swelling pressure
	- Free swell
	 Swell under constant load
Uniaxial compression and	– Value of $\sigma_{\rm C}$
deformability (rock)	- Value of deformation modulus (E)
	- Value of Poisson's ratio (<i>v</i>)
Point-load test (rock)	- Strength index I_{s50}
Direct shear test (rock)	 Stress-displacement curve
	– Mohr diagram
	$-c', \varphi'$
	 Residual parameters
Brazil test (rock)	- Tensile strength ($\sigma_{\rm T}$)
Triaxial compression test	Stress-strain curve(s)
(rock)	Stress paths
	Mohr circles
	- c', φ'
	 Values of deformation modulus (E) and Poisson's ratio (ν)

b See Section 5.

Annex B (Informative)

Planning of geotechnical investigations

B.1 Stages of ground investigations in geotechnical design, execution of works and exploitation of the structure



B.2 Selection of ground investigation methods in different stages

Table B.1— Example of the selection of ground investigation methods in different stages

Preliminary investigations		Design investigations		Control investigations		
Desk study of topographical,	Fine soil CPT, SS, DP, SE		Pile foundation	SS, CPT, DP, SR FVT, SPT, PIL PS, OS, CS, PMT GWC		PIL, Pile driving tests, Stress wave measurements GWC, settlements, Inclinometers
historical, geological and hydrogeological maps Mineral extraction	FVT or SPT OS TP, PS, OS GW	Preliminary choice of foundation method Preliminary choice of foundation method Preliminary choice of foundation method method	Shallow foundation	SS or CPT, DP FVT, DMT or PMT, BJT PS, OS, CS, TP GWC		Check of the soil type Check of the stiffness (CPT) Settlements, Inclinometers, GWC Volume change
Aerial photo - interpretation Archives of previous	Coarse soil SS, CPT, DP, SR_		Pile foundation	CPT, DP, SR SPT, DMT, PIL OS,, TP GWO	control of control of control of ground	potential due to water content change PIL, Pile driving tests Stress wave measurements GWC, settlements Inclinometers
construction works and investigations Site inspection	SPT AS, OS, TP GW		Preliminary choice of foundation	Shallow foundation	CPT,DP SPT, PMT, BJT, DMT, PLT OS, TP GWO	improvement works and stability during construction
Preliminary geophysical surveys Preliminary intrusive investigations	Rock SR, CPT, MWD PLT CS, AS, TP		Pile or shallow foundation	SR, MWD, mapping of discontinuities RDT, PMT, BJT TP, CS GWO		Check inclination and discontinuities in the rock and its surface Check contact between pile toe/ foundation and rock surface Verify water conditions of flow and pressure

1	Abbreviations				
	Field testing		Sampling		
	BJT DP SR SS CPT(U) SPT PMT DMT FVT PLT MWD SE PIL	Borehole jack test Dynamic probing Soil/rock sounding Static sounding (e,g, weight sounding test, WST) Cone penetration test (with pore pressure recording) Standard penetration test Pressuremeter test Dilatometer test Dilatometer test Field vane test Flate load test Measuring while drilling Seismic measurements Pile load test	PS Piston sampler CS Core sampler AS Auger sampler OS Open sampler TP Test pit sampling Groundwater measurements GW Groundwater measurements GWO Groundwater measurements with open system GWC Groundwater measurements with closed system		
	RDT	Rock dilatometer test Notes: Soils include naturally deposited and anthropogenic deposits Surveying and logging are not included in this chart Laboratory tests are not presented on this table			



B.3 examples of recommendations for the spacing and depth of investigations

- (1) The following spacing of investigation points should be used as guidance:
- for high-rise and industrial structures, a grid pattern with points at 15 m to 40 m distance;
- for large-area structures, a grid pattern with points at not more than 60 m distance;
- for linear structures (roads, railways, channels, pipelines, dikes, tunnels, retaining walls), a spacing of 20 m to 200 m;
- for special structures (e.g. bridges, stacks, machinery foundations), two to six investigation points per foundation;
- for dams and weirs, 25 m to 75 m distance, along relevant sections.
- (2) For the investigation depth z_a the following values should be used as guidance. (The reference level for z_a is the lowest point of the foundation of the structure or structural element, or the excavation base.) Where more than one alternative is specified for establishing z_a , the one which yields the largest value should be applied.

NOTE For very large or highly complex projects, some of the investigation points generally extend to greater depths than those specified under B.3 (5) to B.3 (13).

- (3) Greater investigation depths should always be selected, where unfavourable geological conditions, such as weak or compressible strata below strata of higher bearing capacity, are presumed.
- (4) Where structures under B.3 (5) to B.3 (8) and B.3 (13) are built on competent strata, the depth of investigation can be reduced to $z_a = 2$ m, unless the geology is indistinct, in which case at least one borehole should be taken down to a minimum of $z_a = 5$ m. If a bedrock formation is encountered at the proposed base of the structure, this should be taken as the reference level for z_a . Otherwise, z_a refers to the surface of the bedrock formation.
- (5) For high-rise structures and civil engineering projects, the larger value of the following conditions should be applied (see Figure B.1 a)):
- $-z_a \ge 6 \text{ m};$
- z_a ≥ 3,0 b_F .

where $b_{\rm F}$ is the smaller side length of the foundation.

(6) For raft foundations and structures with several foundation elements whose effects in deeper strata are superimposed on each other:

$$z_a \ge 1.5 \cdot b_B$$

where $b_{\rm B}$ is the smaller side of the structure, (see Fig. B.1 b)).

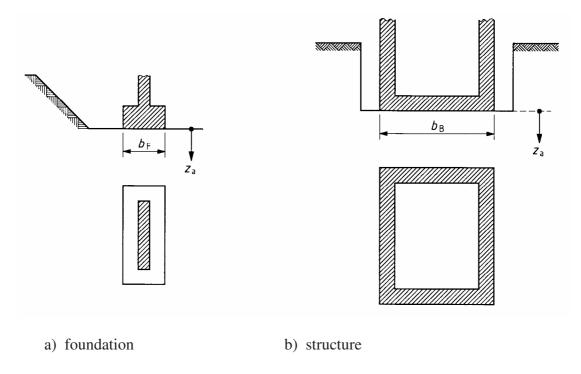


Figure B.1 — High-rise structures, civil engineering projects

(7) Embankments and cuttings, the larger value of the following conditions should be met (see Figure B.2):

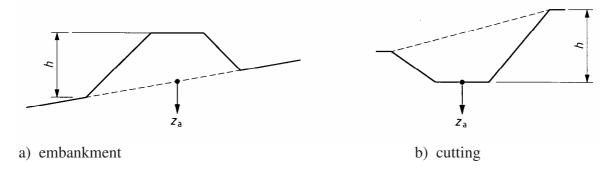


Figure B.2 — Embankments and cuttings

- a) For dams:
 - 0,8h < z_a < 1,2h
 - $z_a \ge 6 \text{ m}$

where h is the embankment height.

- b) For cuttings:
 - $z_a \ge 2,0 \text{ m}$
 - $z_a \ge 0.4h$

where h is the dam height or depth of cutting.

(8) Linear structures, the larger value of the following conditions should be met (see Figure B.3):

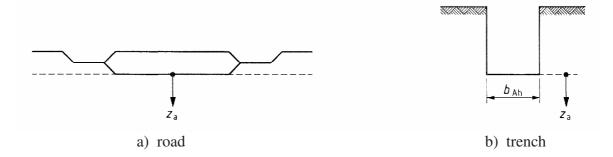


Figure B.3 — Linear structures

a) For roads and airfields:

 $z_a \ge 2$ m below the proposed formation level.

- b) For trenches and pipelines, the larger value of:
 - $z_a \ge 2$ m below the invert level;
 - $-z_a \ge 1.5b_{Ah}$

where b_{Ah} is the width of excavation.

- c) Where relevant, the recommendations for embankments and cuttings should be followed.
- (9) For small tunnels and caverns, (see Figure B.4):

$$b_{\rm Ab} < z_{\rm a} < 2.0b_{\rm Ab}$$

where b_{Ab} is the width of excavation.

The groundwater conditions described in (10) b) should also be taken into account.

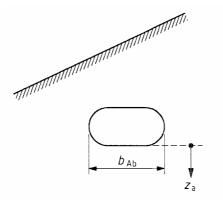


Figure B.4 — Tunnels and caverns

(10) Excavations (see Figure B.5).