

VEHICLE INFORMATION 400 Commonwealth Drive, Warrendale, PA 15096-0001 REPORT

SURFACE

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An American National Standard

AERODYNAMIC TESTING OF ROAD VEHICLES - OPEN THROAT WIND TUNNEL ADJUSTMENT

Foreword—This document has also changed to comply with the new SAE Technical Standards Board format. The document title has also changed.

- Scope—As a simulation of road driving, wind tunnel testing of full-size vehicles produces certain errors in the 1. aerodynamic forces, aerodynamic moments, and surface pressures. The magnitude of these errors, in general, depends on the following:
 - a. Flow quality
 - b. Determination of the reference dynamic pressure
 - c. Wind tunnel floor boundary layer
 - d. Test section geometry and position of the car within that geometry
 - e. Shape of the vehicle
 - Blockage ratio: The ratio of the cross-sectional area of the vehicle to the cross-sectional area of the wind tunnel nozzle
 - g. Wheel rotation
 - h. Internal flow in the model

The SAE Standards Committee, Open Throat Wind Tunnel Adjustments had as a goal to document the knowledge of the influence of model interference on wind tunnel test results for automotive open jet wind tunnels. This document contains the following information related to this subject:

- a. Design data of open throat wind tunnels
- b. A summary of published and unpublished test data
- c. Documentation and theoretical explanation of various blockage correction procedures for automotive
- d. Critical evaluation of blockage correction procedures, especially in relation to other influences, such as test section geometry, position of the car, floor boundary layer, etc.
- e. Recommendation of a calibration procedure to determine the effect of blockage and other influences in each individual wind tunnel

An initial goal of the committee, to recommend a well proven correction procedure for automotive open jet wind tunnels based on blockage theory (Figure 1), could not be established at this time. The reason is that, besides blockage, other factors, such as test section geometry, are at least as influential as pure blockage. As these influential parameters are wind tunnel specific, a general valid adjustment procedure is presently not available.

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Clean Blockage means:

- O no boundary layer effects
- O no nozzle effects
- O no collector/model interaction
- no buoyancy effects (i.e. longitudinal static pressure gradient)

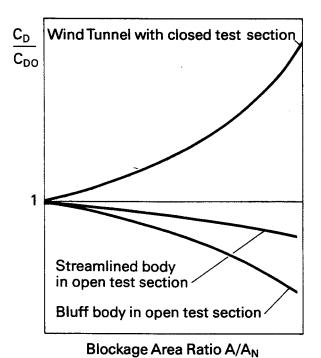


FIGURE 1—PURE MODEL SIZE INFLUENCE

2. References

- **2.1 Applicable Publications**—The following publications form a part of the specification to the extent specified herein. Unless otherwise indicated the lastest revision of SAE publications shall apply.
- 2.1.1 SAE PUBLICATIONS—Available from SAE, 400 Commonwealth Drive, Warrendale, PA 15096-0001.
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- 2. Buchheim, R. et al.
 - Comparison Tests Between Major European Automotive Wind Tunnels.
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- 3. Buchheim, R. et al.

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4. Cogotti, A. et al.

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Blockage Effects in Automotive Wind-Tunnel Testing

SAE Paper 860093/1986

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General Consideration About Blockage Correction in Open Jet Wind Tunnels SAE Subcommittee No. 9 - Communication (1987)

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Paper planned for SAE Congress, Detroit, February 1990

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6. Kuchemann, D., Vandrey, F.

Zur Geschwindigkeitskorrektur in Windkanälen mit freier Meβstrecke unter besonderer Berücksichtigung des Düseneinflusses

Jahrb. 1941 der deutschen Luftfahrtforschung

7. Mercker, E.

A Blockage Correction for Automotive Testing in a Wind Tunnel With Closed Test Section

J. Wind Engineering and Industrial Aerodynamics, 22 (1986)

8. Maskell, E.

A Theory of the Blockage Effects on Bluff Bodies and Stalled Wings in a Closed Wind Tunnel ARC, R & M 3400, 1961

9. Sachs, P.

Wind Forces in Engineering

Pergamon Press, Volume 3, 1972

10. Rogers, E.

Subsonic Wind Tunnel Wall Corrections

AGARDograph 109, 1966

11. Owen, T.B.

Measured Blockage Effects on Bluff Bodies in Closed and Open Wind Tunnels

RAE Technical Report 78151, Dec. 1978, London

12. Templin, J.T., Raimondo, S.

Experimental Evaluation of Test Section Boundary Interference Effects in Road Vehicle Tests in Wind Tunnels

6th Colloquium on Industrial Aerodynamics, June 19-21, 1985, Aachen

13. Gerhardt, H.J., KRAMER, C.

Blockierungseffekte in Windkanälen mit Bodenplatte und offener Meβstrecke Vortrag im HDT im Rahmen des Seminars

Kraftfahrzeugaerodynamik, 11/87

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Aerodynamik von Kraftfahrzeugen, 11/87

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Flow Studies of an Open Jet Wind Tunnel and Comparison With Closed and Slotted Walls Journal of Wind Engineering and Industrial Aerodynamics, 22 (1986), 115–127

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Influence of Test Section Length and Collector Area on Measurements in Three-Fourths Open Jet in Automotive Industry

SATA-Conference No. 23, Palo Alto, CA, 1987

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Haus der Technik Tagung Nr. T-30-905-056-7, Nov. 1987

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Determination of Dynamic Pressure and Reference Pressure in Automobile Wind Tunnels With Open Test Sections

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- 3. Description of Open Jet Automotive Wind Tunnels—For automotive applications, an open jet wind tunnel is a wind tunnel where the test section is three-fourths open and the road is represented by a level floor. For historical reasons (2.1.1 (1) and 2.1.2 (1)), open jet wind tunnels for automotive testing are used mainly in Europe. Their principal advantages are as follows:
 - a. Theoretically lower absolute values of blockage correction compared to closed test sections
 - b. Easy access to the test section

In designing open jet wind tunnels, the control of the flow quality data is a major problem. Based on the available data and the experience of the members of the committee, the flow quality data that are generally sufficient, and (in any case) achievable, in an open jet wind tunnel for automotive testing are given in Table 1.

TABLE 1—FLOW QUALITY FOR OPEN THROAT TEST SECTIONS
- EXISTING MINIMUM REQUIREMENT

| | | Existing Minimum Requirement | | | | | | |
|----------------|-------------------|------------------------------|--|--|--|--|--|--|
| Angularity | Δα | | | | | | | |
| in pitch | (deg) | ≤± 0.5 | | | | | | |
| Angularity | Δβ | | | | | | | |
| in yaw | (deg) | ≤ ± 0.5 | | | | | | |
| Uniformity of | Δv | | | | | | | |
| flow velocity | (%) | ≤ ± 1.0 | | | | | | |
| Turbulence | Tux | | | | | | | |
| intensity | (%) | ≤ 0.5 | | | | | | |
| Pressure Level | Δср | | | | | | | |
| variation | (-) | < 0.01 | | | | | | |
| Length of | Δ1/L | | | | | | | |
| pressure level | (-) | ≥ 1.0 (≥ 1.5) ⁽¹⁾ | | | | | | |
| Displacement | $\delta^{^\star}$ | | | | | | | |
| thickness | (mm) | 10% of the ground clearance | | | | | | |

Some experimental results (Vagt SAE 88) suggest that for larger blockage ratios (>5% – 10%) the length of constant pressure level should be increased.

The test section geometrical parameters of various open jet wind tunnels used for full-scale automotive testing are given in Table 2. Table 3 gives the data for tunnels that are used for scale model testing. The effect of these geometrical parameters is superimposed on blockage effects in open jet wind tunnels, as will be shown later.

TABLE 2—OPEN TEST SECTION GEOMETRY OF LARGE TUNNELS (FOR FULL-SCALE TESTING)

| WT Owner | | | | | | | | | | |
|-----------------------------|-----------|--------|--------|-------|------|-------|---------|---------|------|-------|
| WT Part | Dimension | BMW AE | BMW AC | DB | FIAT | FORD | PININF. | PORSCHE | VW | IVK |
| Nozzle Exit Area | m^2 | 20.02 | 10.0 | 32.64 | 30.0 | 23.75 | 11.75 | 22.3 | 37.5 | 22.45 |
| Nozzle Width | m | 5.77 | 4.0 | 7.4 | 7.0 | 6.0 | 5.0 | 6.2 | 7.5 | 5.8 |
| Nozzle Height | m | 3.47 | 2.828 | 4.9 | 4.6 | 4.0 | 2.9 | 3.6 | 5.0 | 3.87 |
| Nozzle Contraction Ratio | - | 3.66 | 3.0 | 3.6 | 4.0 | 4.0 | 6.5 | 6.06 | 4.0 | 4.411 |
| Test Section Length | m | 10.02 | 9.83 | 10.0 | 10.5 | 10.5 | 8.0 | 13.5 | 10.0 | 9.5 |
| T-S Surr. Bound. Width | m | 10.34 | 13.74 | 14.8 | 12.2 | 15.0 | 9.6 | 12.7 | 17.0 | 15.0 |
| T-S Surr. Bound. Height | m | 5.30 | 5.72 | 7.5 | 10.8 | 8.5 | 4.2 | 6.85 | 13.0 | 8.5 |
| Model. Ref. Point x/L (TS) | - | 0.471 | 0.356 | 0.5 | 0.55 | 0.39 | 0.46 | 0.41 | 0.43 | 0.474 |
| Collector Cross Section | m^2 | 22.12 | 22.64 | 47.4 | 40.5 | 29.73 | 17.33 | 42.2 | 44.8 | 26.5 |
| Collector Width | m | 6.01 | 5.66 | 8.5 | 7.8 | 6.68 | 6.2 | 8.7 | 8.0 | 6.354 |
| Collector Height | m | 3.68 | 4.0 | 6.5 | 5.6 | 4.45 | 3.5 | 4.85 | 5.6 | 4.166 |
| Maximum Speed | m/s | 50 | 70 | 70 | 56 | 51 | 54 | 64 | 50 | 75 |

TABLE 3—OPEN TEST SECTION GEOMETRY OF SMALL TUNNELS (FOR SCALE MODEL TESTING)

| WT Owner | | | | | | | | | | | | | |
|------------------------------|----------------|--------|--------|-------|-------|------|------|------|-------|-------|---------|-------|------|
| WT Part | Dimen- sion | Aachen | Aachen | DB | DLR | DLR | DLR | FIAT | FORD | IVK | PORSCHE | VOLVO | vw |
| Nozzle Exit Area | m^2 | 1.0 | 2.69 | 1.64 | 8.61 | 8.1 | 1.53 | 4.0 | 8.64 | 1.654 | 1.4 | 4.125 | 6.0 |
| Nozzle Width | m | 1.1 | 2.0 | 1.5 | 3.25 | 3.0 | 1.3 | 2.4 | 3.65 | 1.575 | 1.55 | 2.4 | 3.0 |
| Nozzle Height | m | 1.1 | 1.4 | 1.096 | 2.65 | 2.7 | 1.18 | 1.7 | 2.44 | 1.05 | 0.9 | 1.73 | 2.0 |
| Nozzle Contraction Ratio | - | 3.3 | 2.57 | 6.0 | 5.6 | 5.44 | 4.91 | 7.0 | 11.0 | 4.988 | 6.06 | 6.25 | 6.0 |
| Test Section Length | m | 1.83 | 4.0 | 2.8 | 6.0 | 6.0 | 2.48 | 4.0 | 6.1 | 2.578 | 3.38 | 8.82 | 6.0 |
| T-S Surr. Bound. Width | m | 8.65 | 5.74 | 5.15 | 16.4 | 8.0 | 4.8 | 5.7 | 15.0 | 6.85 | 3.42 | 6.06 | 6.5 |
| T-S Surr. Bound. Height | m | 4.0 | 2.85 | 2.35 | 9.5 | 5.9 | 5.2 | 6.4 | 8.5 | 3.39 | 1.84 | 4.0 | 4.0 |
| Model Ref. Point x/L (TS) | - | 0.55 | 0.38 | 0.46 | 0.43 | 0.48 | 0.5 | 0.4 | 0.41 | 0.474 | 0.41 | 0.283 | 0.42 |
| Collector Cross Section | m^2 | 1.45 | 4.2 | 2.3 | 10.26 | 17.0 | 1.84 | 7.6 | 11.33 | 1.921 | 2.66 | 12.25 | 6.9 |
| Collector Width | m | 1.32 | 2.4 | 1.85 | 3.67 | 5.15 | 1.5 | 3.3 | 4.12 | 1.712 | 2.18 | 3.5 | 3.0 |
| Collector Height | m | 1.32 | 1.7 | 1.3 | 2.8 | 3.3 | 1.28 | 2.3 | 2.75 | 1.122 | 1.22 | 3.5 | 2.3 |
| Maximum Speed | m/s | 42 | 38 | 65 | 75 | 65 | 55 | 70 | 84 | 80 | 64 | 53 | 50 |

The data given in Tables 1, 2, and 3 are also an indication of the range of flow quality and test section design data for which the following discussions about blockage corrections are valid. The data are based on the present experience of the committee members. The definition of the various values is as follows:

a. Standard Control Box Test Volume: All flow quality parameters will be related to a standard control box test volume. The test volume size is defined as:

Length = 100% of typical vehicle length

Height = 100% of typical vehicle height

Width = 100% of typical vehicle width for nonyawed conditions

= 200% of typical vehicle width for yawed conditions